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Title: R&D Lattice Modeling, Manufacturing, and Inspection

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R&D Lattice Modeling, Manufacturing, and Inspection

Masters Degree Final Presentation



Graham Arinder

03/30/2020





Slides Outline



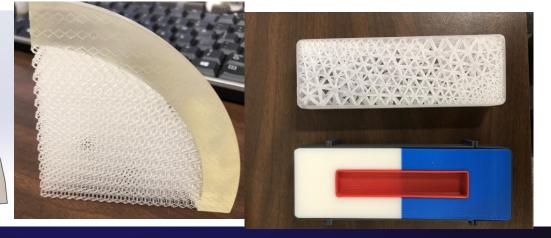
- Project Background
- Lattice Fundamentals and Basic Research
 - Maxwell Criterion
 - Approximations and Analytical Lattice Solutions
 - Testing
 - Testing Results v. Analytical solutions
- Materials, Methods, Modeling, and Inspection
 - Polymers and Metals
 - Additive Processes and Limitations
 - Limitations of Modeling
 - Inspection techniques and Limitations

Project Background

- Mechanical mocks are useful when substituting components in tests of Large assemblies, when that component isn't specifically being tested.
 - Useful when components are rare, expensive, or hazardous and can be replaced in the test
- Simplest mocks match mass properties. More complex mocks match mechanical properties as well.
 - Varying wall thickness, lattice density, and unit cell changes response while keeping mass the same

We are asking how to make responses match instead of how low can

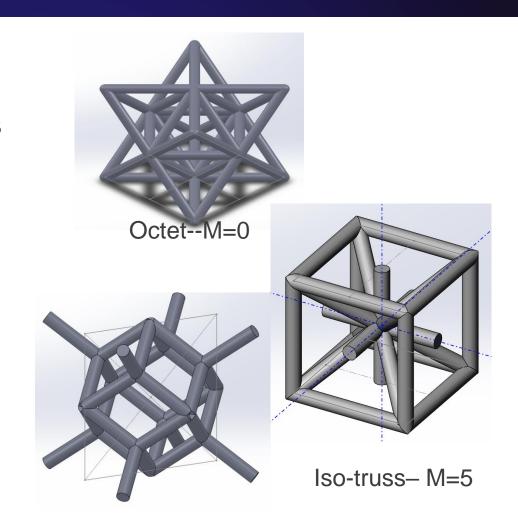




Lattice Fundamentals and Basic Research

Lattice Fundamentals-Stretch vs. Bend Dominated

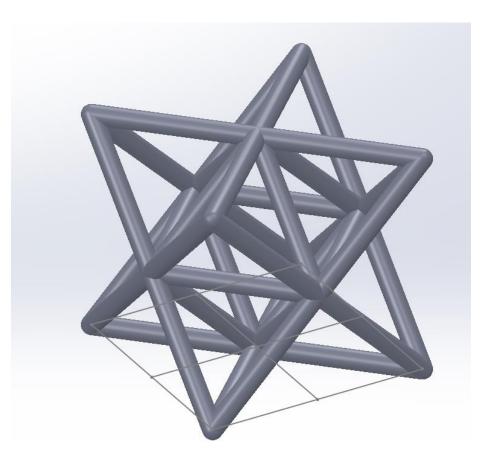
- Lattices can be divided into Stretch and Bend dominated
- Division is based on the results of the 3D Maxwell Criterion [1]
 - -M=b-3*j+6
 - b is the number of struts (beams)
 - j is the number of joints
 - If M is greater than or equal to 0 the lattice is stretch dominated.
 - Lattice is self-supporting if pin joint assumption is made
 - Struts are primarily in tension and compression
 - If M is less than 0, the lattice is bend dominated
 - Lattice is not self-supporting with pin joint assumption
 - Struts are primarily in bending



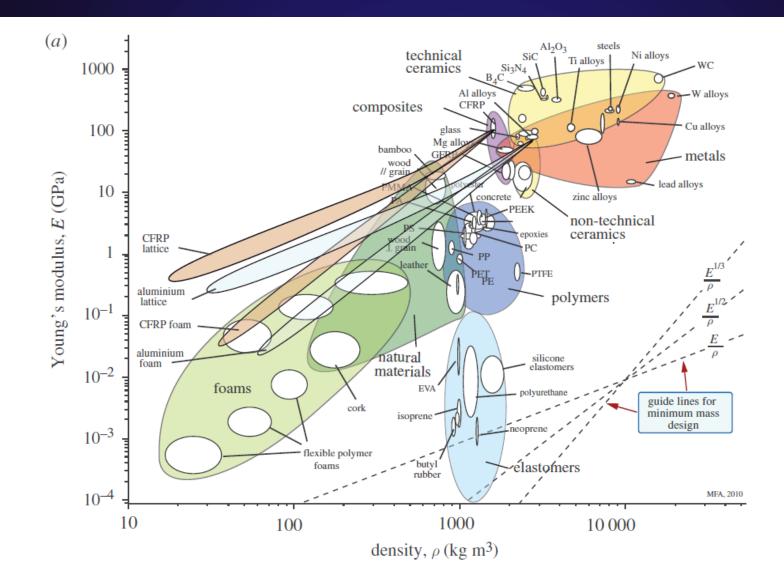
Rhombic Dodecahedron M=-4

Lattice Fundamentals-Maxwell Criterion example

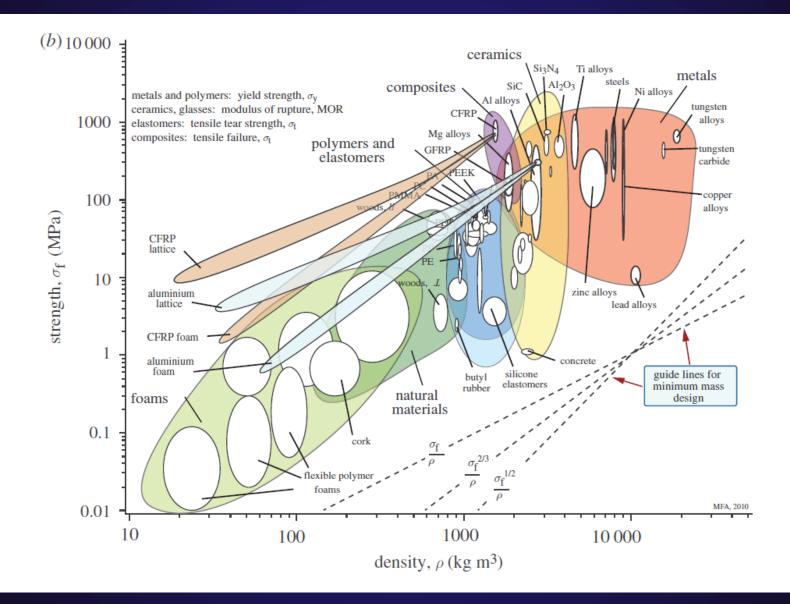
- The octet unit cell has
 - -b=36
 - -j=14
- M=b-3*j+6
- M=0
- Octet is statically determinate
- Using the pin joint assumption, octet could be solved using the method of joints from statics.



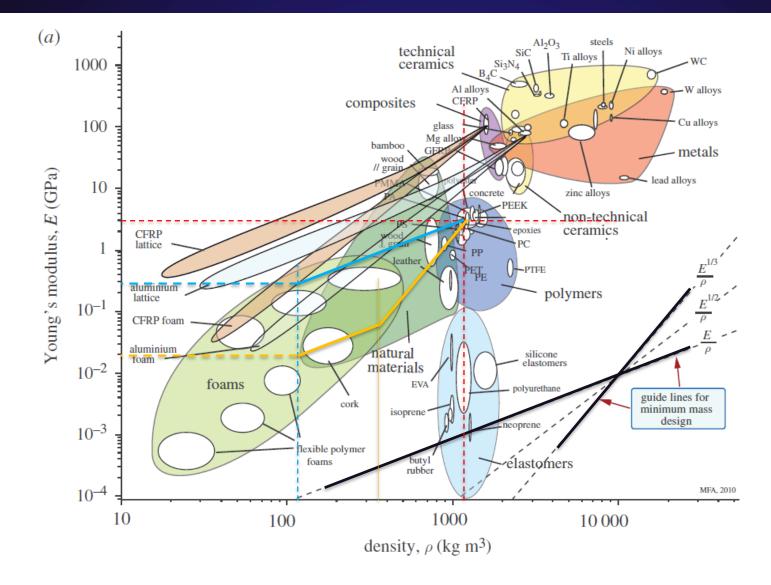
Effective Modulus and Strength-Ashby chart [2]



Effective Modulus and Strength-Ashby chart [2]



Ashby Chart Example—10% Octet Lattice, Formlabs Clear SLA Resin (ρ=1200 kg/m³, E=2.8 Gpa) [2]



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Effective Modulus and Strength-Octet analytical solutions

 From Messner "Wave propagation" [3] The approximate relative density for an octet lattice is given by:

$$-\bar{\rho} = \frac{6\sqrt{2}A}{l^2}$$

- Where A is cross sectional area of the strut, I is length of the strut,
- This equation assumes that the volume of the nodes negligible.
- The effective modulus for an octet lattice with a load applied on an axis can be gained from Messner's stiffness tensor and is:

$$-E_{eff} = \frac{E\overline{\rho}}{6}$$

- This equation assumes that the octet nodes are pin jointed, and therefore, cannot sustain a moment.
- Valid for low relative densities (<10%)

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Effective Modulus and Strength-Octet analytical solutions

Deshpande claims in "Effective properties of the octet-truss lattice" [1]
 that the effective modulus is:

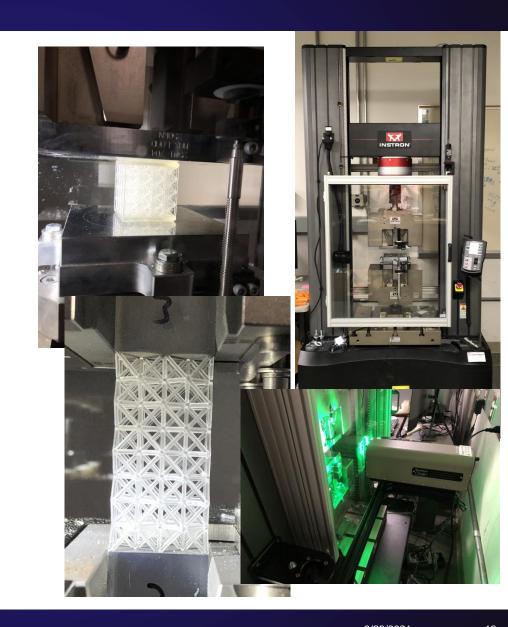
$$-E_{eff} = \frac{E\overline{\rho}}{9}$$

- However, in his compliance tensor a few lines later, the effective modulus simplifies to $E_{eff}=\frac{E\overline{\rho}}{6}$
- Since this paper contains conflicting information, Messner's work is used
- An equation that estimates the strength of an octet lattice can be gained from Fig. 3 of "Effective properties of the octet-truss lattice" paper as well.

$$-\sigma_{eff} = \frac{\sigma_y \overline{\rho}}{3}$$

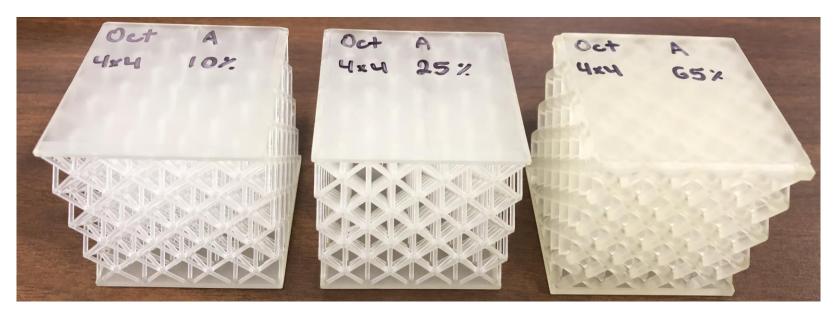
Experimental Setup

- Instron 5985 Dual column test frame with 250 kN capacity
- EpsilonOne Non-contact extensometer gauge length of 10-50mm (class B-1)
- Compression specimen
 - -2" cube with 0.5" unit cells (SLA)
 - 2" cube 4.2 mm unit cells (Ti-5533)
 - **10%**, 25%, 65%
- Tensile specimens
 - -1"x1"x2" test section
 - Same lattice properties as compression



Effective Modulus and Strength-Actual Results

Actual Octet Compression Results v. Approximations and Analytical solutions Formlabs Clear SLA Resin (MPA)					
		A		==.	I ANII 4
Relative density	Messner	Ashby chart M1	Ashby chart M2	LANL FEA	LANL tests
10%	38.3	280	20	32.4	31.4
25%	95.8	800	50	106.4	129.7
65%	249.2	1900	480	545.9	628.8



Materials, Processes, Modeling, and Inspection

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Materials—AM Polymer

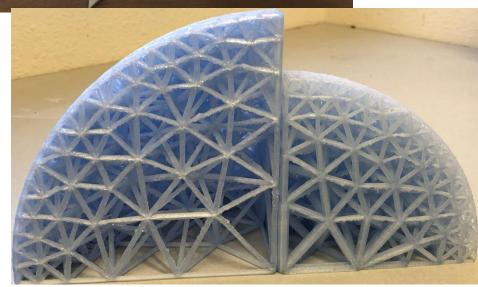
SLA resin

- High detail prints
- Isotropic behavior
- Can be "doped" with different materials to change properties (density, modulus, conductivity)
 - Tungsten, hollow glass spheres, chopped glass and carbon fibers
- Occludes at high density (>65%) and small cell size (~3mm)
- Limited to smaller build volumes (5" cube is common, larger available)

• FDM

- Low detail compared to SLA
- Anisotropic behavior ~10% weaker along build layers
- Soluble support allows for long unsupported strut lengths
- Many unfilled and filled materials commercially available
- Very large build volumes are possible
 - Up to 36"x24"x36" at LANL with soluble support





Materials—Metals, Laser Powder bed

Ti-6Al-4V

- Large Body of research on properties of AM material
- Areas of high stress cause distortion and build failures, especially on small diameter struts, porosity

• Ti-5Al-5V-5Mo-3Cr

- Less prone to distortion than Ti-64
- Typically has higher yield strength

Other Materials of interest

- 316/316L Stainless
- Aluminum Alloys (AlSi10Mg, A360)
- Copper







Lattice Types

• Octet

- Orthotropic Stretch Dominated Lattice (M=0)
- Has horizontal struts

• Iso-truss

- Projected to have nearly isotropic behavior
- Stretch dominated (M=5)

Unstructured Tetrahedral

- Stretch Dominated (M=3?)
- Conformal geometry easily produced from FEA meshes

Rhombic Dodecahedron

- Bend Dominated (M=-4)
- Has no horizontal or low angle struts

• Other Lattice Types

- CORC—(M=-54), but approaches stretch dominated properties
- Myriad of Cubic Cells
- Other unit cell base shapes
 - · Hexagonal Close packed

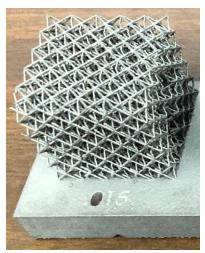




Printing Limitations

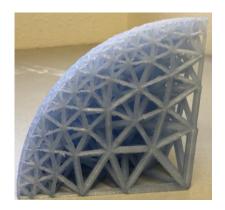
Metal

- Maximum Part Size-~400mm cube
- Maximum unsupported horizontal length-~3-6mm
- Minimum angle for unsupported struts-~45deg
- Minimum strut Diameter-~350um
 - · Laser width
 - Strut warp/ catch by recoater blade
- Minimum/Maximum practical relative density ~8%-65%
- Anisotropy in printing process
- Cleaning out powder and parasitic material
- Strut warping/broken struts



Polymer

- Max part size
 - SLA-5.7"x5.7"x7.3 inches (larger is possible)
 - FDM- Up to 36"x24"x36"
- Maximum unsupported horizontal length
 - SLA~.5"(dependent on strut diameter)
 - FDM- nearly unlimited with use of soluble support
- Minimum Strut Diameter
 - SLA~125 um
 - FDM~1.5mm
- Minimum/Maximum Relative Density
 - SLA-<5%-65%
 - FDM
- Material warping
- Resin Occlusion
- Broken Struts



Design and manufacturing Software Limitations

CAD Programs

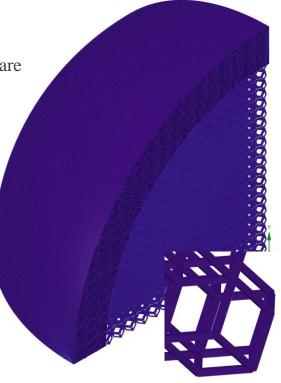
- Solidworks
 - Primarily single threaded application therefore it bogs down significantly as part size increases.
 - 3" hemisphere is the largest successfully made part in Solidworks
 - Solidworks had significant issues with the part and crashed many times
 - Only able to generate non-conformal lattices so far
 - Currently limited to single cell size/density and geometry
- Kansas City National Security Campus Geometry Conformal Lattice Software
 - Generates conformal lattice structures
 - Still under development
 - Limited unit cells.

TO Programs

- Ansys will create lattices, but unit cells are limited to their predefined cells.
 - Can create variable density lattices based on Ansys TO resultes
- Octet is the only cell from the earlier list that is available for use
- All available lattices have horizontal struts

Slicing Software

- CAD programs tend to leave artifacts in STL file when exporting lattices
- Programs hang or crash with large STL sizes
- Many are single threaded when generating support and tool paths.
- 1/8 sphere took over 24 hours to generate and is 35 MB, square struts used to reduce size



Inspection Limitations

Weight/relative density

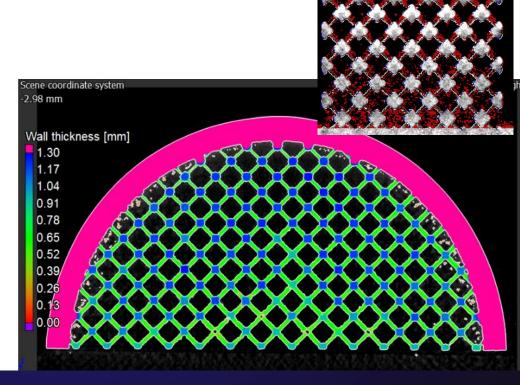
- Few limitations in measuring weight and volume
- If doing a submerged volume test, must make sure all air is removed from lattice structure

Optical Scanning

- Only capable of inspecting visible struts in the first few layers of cells
- Cannot see the back side of struts so assessing the roundness of a strut would be difficult

CT Scanning

- Noise caused by x-ray scatter
 - Orange disconnected blobs in image
- Lack of penetration in metals
 - Voids at lattice nodes
- Part envelope of 20-30" machine dependent
- High density parts require higher power which reduces scan resolution
- For Ti parts, max practical size may be
 only 6-8" in diameter (with current equipment)
- Images must be meticulously studied for flaws
 - May be possible to automate this process.
- Other internal imaging techniques may be possible

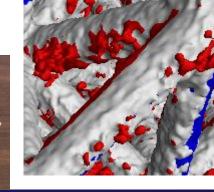


References

- [1] Deshpande, V. S., Fleck, N. A., & Ashby, M. F. (2001). Effective properties of the octet-truss lattice material. *Journal of the Mechanics and Physics of Solids*, *49*(8), 1747-1769
- [2] Fleck, N. A., Deshpande, V. S., & Ashby, M. F. (2010). Micro-architectured materials: past, present and future. *Proceedings of the Royal Society A: Mathematical, Physical and Engineering Sciences*, 466(2121), 2495-2516.
- [3] Messner, M. C., Barham, M. I., Kumar, M., & Barton, N. R. (2015). Wave propagation in equivalent continuums representing truss lattice materials. *International Journal of Solids and Structures*, 73, 55-66.

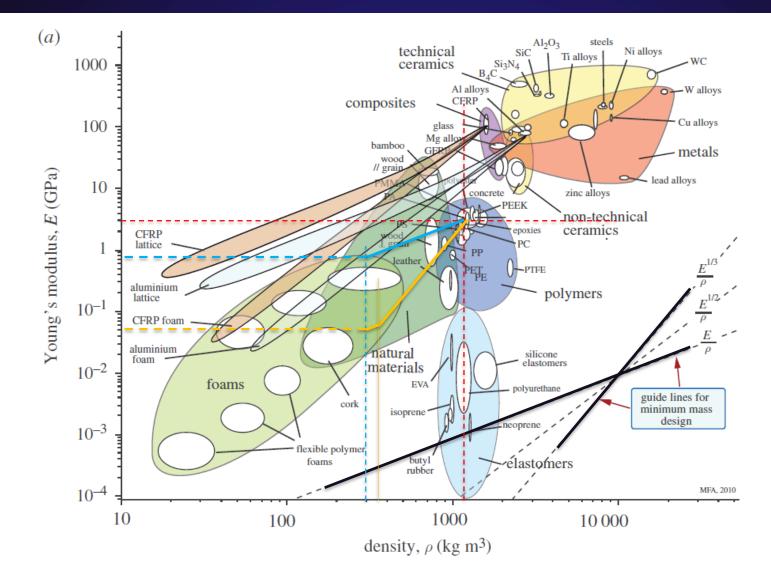
Questions?







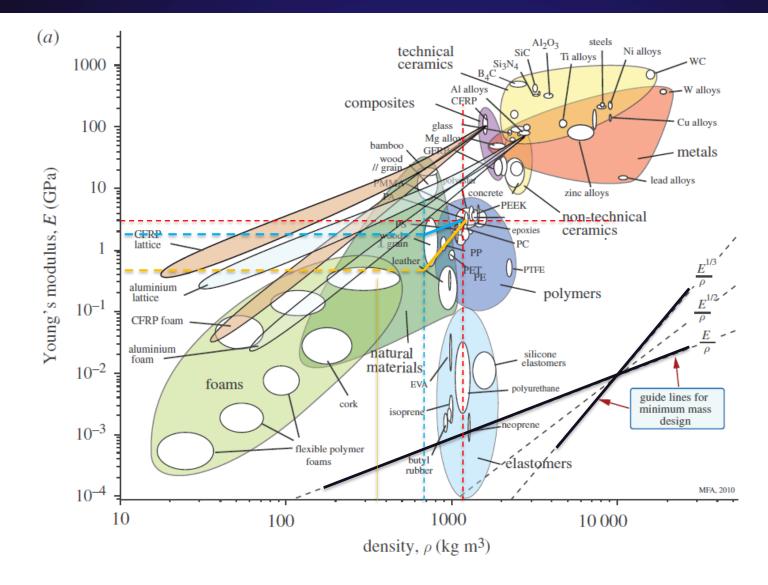
Ashby Chart Example—25% Octet Lattice, Formlabs Clear SLA Resin (ρ=1200 kg/m³, E=2.8 Gpa) [2]



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Ashby Chart Example—10% Octet Lattice, Formlabs Clear SLA Resin (ρ=1200 kg/m³, E=2.8 Gpa) [2]



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